

## A Continuous Stochastic Disaggregation Model of Rainfall for Peak Flow Simulation in Urban Hydrologic Systems

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### Abstract

In the paper by Durrans *et al.* (1999), an algorithm proposed by Ormsbee (1989) is recommended for the stochastic disaggregation of hourly rainfall in continuous flow simulation studies of urban hydrologic systems. However, Durrans *et al.* found that the method produced a “severe negative bias” in the maximum rainfall intensity of the disaggregated series, so that peak flows in urban systems are likely to be under-estimated by the model. Here we develop a method for disaggregating hourly data to 5min series, which addresses the problem of negative bias. A regression equation is derived for the ratio of the maximum 5min depth to the total depth in the hour. Thus, for any given hourly depth this ratio can be simulated and multiplied by the hourly depth to obtain a 5min maximum. The temporal location of the maximum within the hour can be randomly placed using an appropriate distribution function, e.g. based on a geometrical construction as developed by Ormsbee (1989). The model is developed and tested using 5min rainfall data taken from Lund (1923-39) and Torsgatan (1984-93), Sweden. The results support the use of the model in urban drainage applications.

### Introduction

As part of a UK Urban Pollution Management Programme, initiated by the Water Research Centre (e.g. see Tyson and Clifforde 1989, or Crabtree 1988), Cowpertwait *et al.* (1996*a,b*) developed a regionalised stochastic rainfall generator. This generator incorporates a Neyman-Scott point process model for the simulation of hourly rainfall (e.g. see Cowpertwait, 1998), and an algorithm proposed by Ormsbee (1989) for stochastically disaggregating the generated hourly data into 5min values. The generator has been further developed for use in Sweden as part of a European Union Technology Validation Project (Threlfall *et al.*, 1998, 1999). In this paper, we present results from that project which help address the problem of negative bias in the maximum intensities of the disaggregated rainfall, recently reported by Durrans *et al.* (1999).

The proposed method uses a regression model to predict the ratio of the maximum 5min depth to the hourly depth, thus enabling a 5min maximum to be simulated for any given hourly depth. The distribution function proposed by Ormsbee (1989) can be used to assign the maximum to a 5min interval within the hour. The model is appropriate for problems in urban wastewater management, as it is likely to give representative peak flows in hydrologic models of sewer networks (Threlfall *et al.*, 1998, 1999). The same methodology could be applied to disaggregate hourly data to intervals smaller or larger than 5 minutes (e.g. one-minute series or 15-minute series).

### Data

Time-series data, of one-minute resolution, were provided by the Danish Hydraulic Institute. The data came from two sites in Sweden (Lund, 1923-39, and Torsgatan, 1984-93) and were aggregated to 5min and hourly series. As we were interested in the more intense rainfall, those hours having a total depth greater than (or equal to) 5mm of rain were extracted together with the maximum 5min depth in the hour. This resulted in 2269 pairs of hourly depths and maximum 5min rainfalls. The ratio  $Y$  of maximum 5min depth to the hourly total was calculated for all the extracted pairs.

### Formulation of regression model

An appropriate regression model for the ratio  $Y$  should contain information known about  $Y$  (e.g.  $0 \leq Y \leq 1$ ) and include possible explanatory variables (e.g. seasonal indicator variables). We thus proposed the following model:

$$Y_i = \left\{ 1 + \exp \left( c_0 + \sum_{j=1}^{11} c_j I_{ij} + Z_i \right) \right\}^{-1}, \quad (1)$$

where  $Y_i$  is the  $i$ th ratio ( $i = 1, \dots, 2269$ ),  $c_j$  are regression coefficients ( $j = 0, 1, \dots, 11$ ), and  $Z_i$  is the  $i$ th residual error. The  $I_{ij}$  are indicator variables taking the values:  $I_{ij} = 1$ , when the  $i$ th ratio is in the  $j$ th season, or  $I_{ij} = 0$ , otherwise. Note that the model has 12 seasons corresponding to each calendar month (with '1' corresponding to January, '2' to February, etc); with only eleven indicator variables being needed because of the constant term  $c_0$ .

In order to estimate the coefficients  $c_j$ , the ratio  $Y$  was transformed using a logit transformation to give the predictor variable  $Y'$  given by:

$$Y'_i = \ln(Y_i^{-1} - 1) = c_0 + \sum_{j=1}^{11} c_j I_{ij} + Z_i \quad (2)$$

The estimation of the coefficients  $c_j$  therefore reduces to fitting a linear regression model which is achieved by least squares estimation. Note that  $E(Z_i) = 0$ , so that predicted values of  $Y'$  will be unbiased.

Conversely, the predicted values of  $Y$  will be biased because of the transformation  $Y = (1 + e^{Y'})^{-1}$ . However, this is of no concern here because we will *simulate* values of  $Y$ , which will be unbiased under the transformation.

The least squares estimates of the coefficients  $c_j$  are shown in Table 1, where it can be seen that there is a slight difference in the predicted ratios for summer and winter, with summer months tending to have higher predicted ratios and, therefore, more high-intensity 5min rainfalls. This reflects the well-known meteorological observation that more frequent high-intensity convective storms occur during summer months, with more low-intensity frontal storms occurring in winter.

Table 1

Fitted regression coefficients and statistical tests\*

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Coefficient	Estimate	SD	T	P
C <sub>0</sub>	1.96	0.520	3.77	0.000
C <sub>4</sub>	-0.995	0.735	-1.35	0.178
C <sub>5</sub>	-1.16	0.559	-2.07	0.039
C <sub>6</sub>	-1.20	0.539	-2.23	0.026
C <sub>7</sub>	-1.04	0.526	-1.97	0.050
C <sub>8</sub>	-0.945	0.528	-1.79	0.075
C <sub>9</sub>	-0.784	0.532	-1.47	0.142
C <sub>10</sub>	-0.617	0.544	-1.13	0.258

$$\sigma_z = 0.735$$

\* Coefficients not listed are estimated as zero

From Table 1, the equation for simulating a ratio of the maximum 5min depth to the hourly depth is given by:

$$Y = \{1 + \exp(2.0 - 1.0 I_4 - 1.2 I_5 - 1.2 I_6 - 1.0 I_7 - 0.95 I_8 - 0.78 I_9 - 0.62 I_{10} + Z)\}^{-1} \tag{3}$$

where  $Z$  is a simulated Normal random variable with mean zero and standard deviation 0.735 (the subscript  $i$  has been omitted without loss of generality). The fitted regression model (3) only explained about 6% of the variation in the data, so that a reasonable approximation can be obtained by neglecting the seasonal indicator variables, i.e. using the model:

$$Y = \{1 + e^Z\}^{-1} \tag{4}$$

where  $Z$  is approximately Normally distributed with mean 1.3 and standard deviation 0.77.

An analysis of the residual errors in the fitted model (2) revealed a slight departure from the Normal distribution in the far tail of the probability plot (Figure 1). This may result in some underestimation of the very extreme 5min intensities when using the Normal distribution. A possible alternative would be to use the empirical distribution of the residuals in simulation, but this would clearly restrict the simulation to past historic values only.

Normal Probability Plot of the Residuals

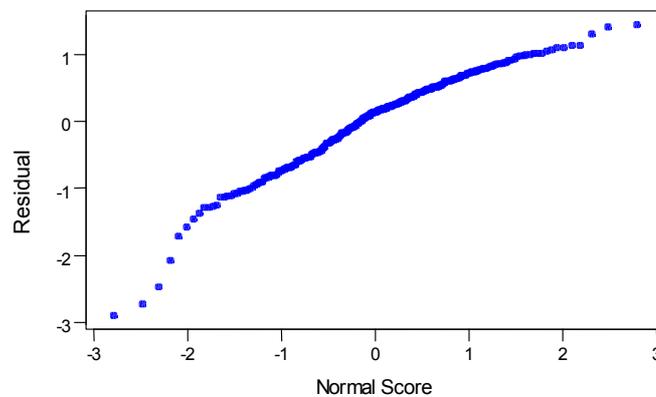


Figure 1: Probability plot for the residual errors in the fitted regression model

Inclusion of site indicator variables, to allow for different ratios at the two sites, had the effect of increasing the residual standard deviation (from 0.735 to 0.736), suggesting that the model can be applied without site indicator variables. This supports the argument that most of the variance in rainfall over a geographical region is explained by data sampled at time intervals greater than 5 minutes. Hence, it is reasonable to hypothesize the use of the same fitted disaggregation model at other urban sites not used in the fitting procedure.

**Stochastic Disaggregation**

Hourly rainfall can be disaggregated into 5min values using the fitted regression model with an appropriate probability distribution for assigning rain within the sub-hourly intervals. The steps below use the fitted model with the probability distribution function proposed by Ormsbee (1989).

- (1) A ratio  $y$  is simulated using equation 3 (or 4) with a simulated Normal random variable  $z$ .

- (2) The simulated ratio is multiplying by the hourly rainfall depth  $x$  (mm) to obtain a simulated maximum 5min depth ( $xy$ ). The remainder  $(1 - y)x$  will be distributed over the hour using pulses of depth 0.01mm, i.e.  $100(1 - y)x$  pulses (see step 8 below).
- (3) The probabilities mass function ( $p_1, p_2, \dots, p_{12}$ ) is found using an appropriate method, e.g. the geometrical construction proposed by Ormsbee (1989), where  $p_i$  is the probability that a depth (or 'pulse') of rain falls in the  $i$ th interval ( $i = 1, \dots, 12$ ;  $p_1 + p_2 + \dots + p_{12} = 1$ ).
- (4) The cumulative distribution function  $F(i) = p_1 + p_2 + \dots + p_i$  is found for each 5min interval in the hour ( $i = 1, \dots, 12, F(0) = 0, F(12) = 1$ ).
- (5) A uniform  $U(0,1)$  random number is generated to determine which interval to assign the maximum 5min depth. For example, if  $F(i-1) < U < F(i)$ , the depth is assigned to the  $i$ th interval ( $i = 1, \dots, 12$ ).
- (6) The probability mass function in step (3) is modified to ensure no pulses of rain fall in the same interval as the maximum 5min depth. For example, if the maximum depth falls in the  $i$ th interval, the following re-assignments are made:  $p_{i+1} \rightarrow p_{i+1} + \frac{1}{2} p_i$ ,  $p_{i-1} \rightarrow p_{i-1} + \frac{1}{2} p_i$ , after which  $p_i \rightarrow 0$  ( $i = 2, 3, \dots, 11$ ). For  $i = 1$ ,  $p_{i+1} \rightarrow p_{i+1} + p_i$  and  $p_i \rightarrow 0$ . For  $i = 12$ ,  $p_{i-1} \rightarrow p_{i-1} + p_i$  and  $p_i \rightarrow 0$ .
- (7) The cumulative distribution function  $F$  is modified using the modified probability mass function in (6) above.
- (8) A uniform  $U(0,1)$  random number is generated and used with the distribution function  $F$  to determine which interval to assign a 0.01mm pulse of rain. This is repeated for each of the  $100(1 - y)x$  pulses (from 3 above). Note that if  $100(1 - y)x$  is a non-integer, then the decimal part  $d$  (mm) can be added to the first pulse to give a depth of  $0.01+d$  (mm). In the unlikely event of an interval reaching the same level as the maximum, the probability for that interval can be assigned to zero and adjustments made to the probabilities for the adjacent intervals (as in 6 above).
- (9) Steps (1) to (8) are repeated for each hour in the series to be disaggregated.

The above procedure ensures that the total hourly depth remains unchanged. In addition, Step 6 allows for some increase in intensity near the maximum in an attempt to preserve the autocorrelation expected in a 5min rainfall time series.

### Tests on the model

To test the model, we selected two historical events from the Lund data: (i) the event having the largest total volume of rain (the 'heaviest event'), and (ii) the event having the highest hourly intensity. Each of these events were aggregated to hourly time series and then disaggregated using the steps above.

For each event, time-series plots of the historical and disaggregated series were found and are given in Figures 2 and 3, where it can be seen that the disaggregation algorithm generates storm profiles which have a realistic appearance, representative of the historical events.

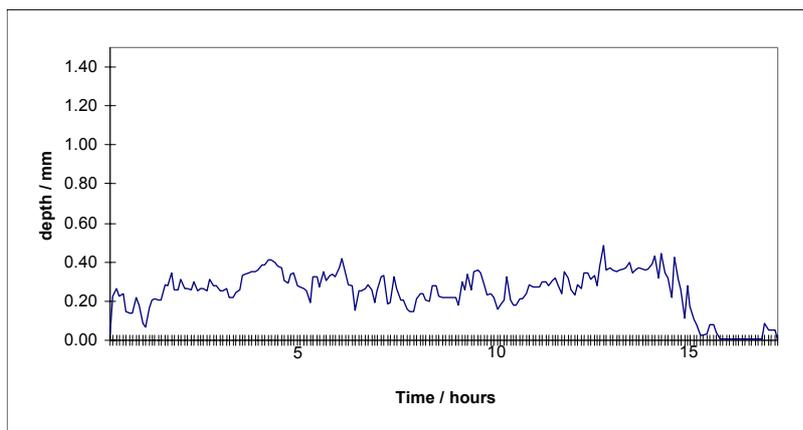


Figure 2a: Time-series plot of the heaviest historical event (Lund, 1923-39)

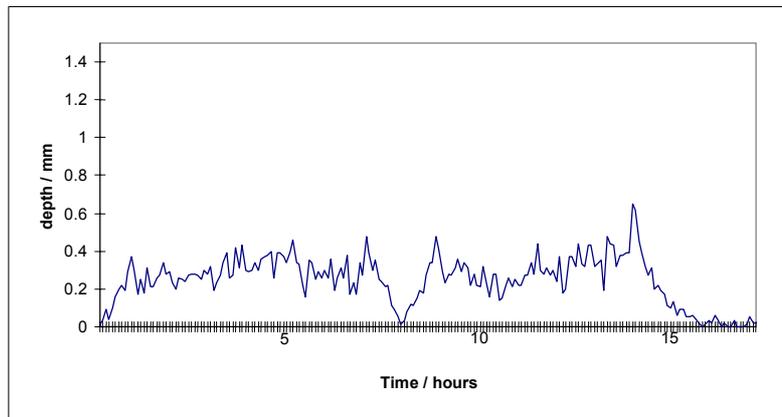


Figure 2b: Time-series plot of the heaviest event when disaggregated

To provide more quantitative tests, sample statistics were evaluated for the historical and disaggregated series. These included the mean, standard deviation (SD), lower quartile (Q1), and upper quartile (Q3). In addition, the sample autocorrelation for a range of lags (the ‘correlogram’) was also found for each event.

Table 2 gives the sample statistics, where it can be seen that a reasonable fit is obtained to the historical values. In particular, the historical standard deviations are well matched by the simulated data even though they have not been used in the fitting procedure. A very slight under-estimation (of 0.05mm) in the distribution tail (Q3) is evident for the most intense event, but this is not likely to be of practical importance.

Table 2: Sample Statistics taken from Historical and Disaggregated Series

Statistic (mm)	Heaviest Event		Most Intense Event	
	historical	Disaggregated	historical	Disaggregated
mean	0.25	0.24	0.32	0.32
SD	0.11	0.13	0.49	0.47
Q1	0.20	0.17	0.04	0.06
Q3	0.33	0.34	0.37	0.32

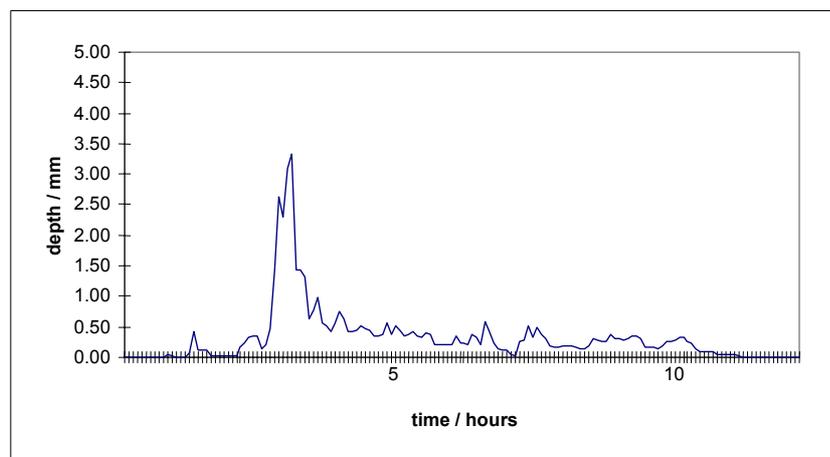


Figure 3a: Time-series plot of the most intense historical event (Lund, 1923-39)

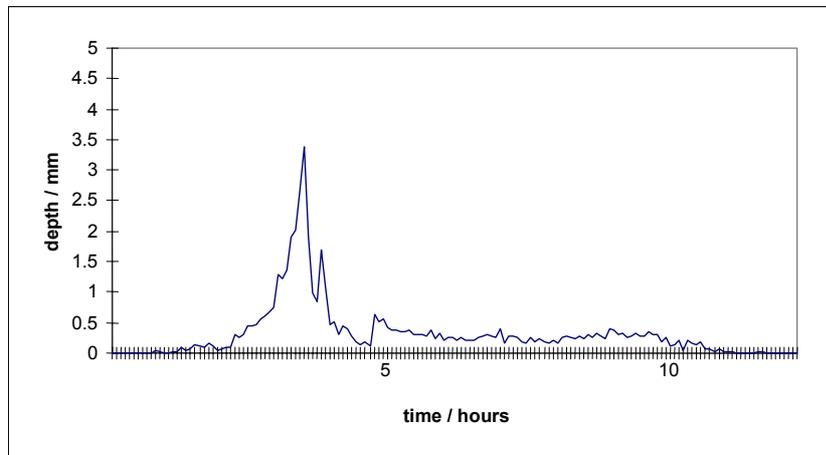


Figure 3b: Time-series plot of the most intense event when disaggregated

The correlograms (Figures 4 and 5) show a satisfactory representation of the correlation structure found in the historical events. For both events, the simulated and historical autocorrelations are approximately equal at lags 1 and reach zero at about the same lag. This is a very good result, particularly given that the disaggregation model does not use correlation in the fitting procedure, as in the case of traditional time-series models (e.g. ARIMA models).

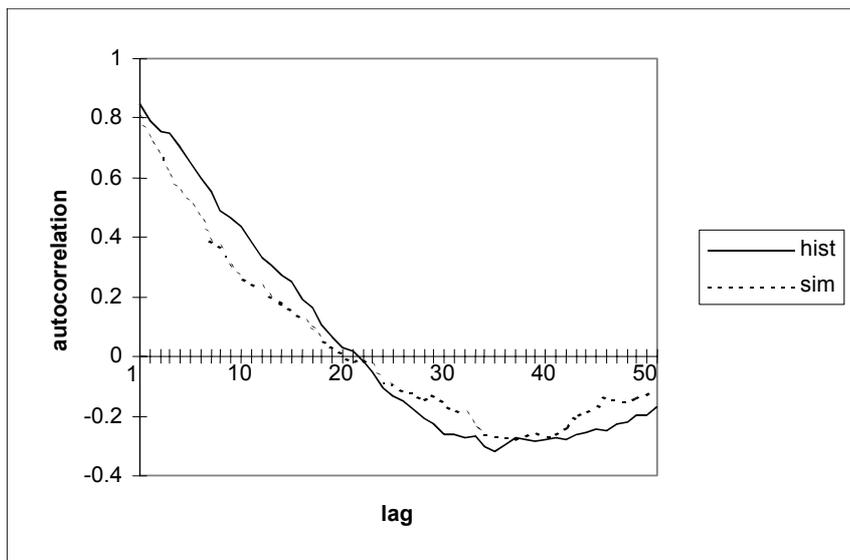


Figure 4: Correlogram of heaviest event

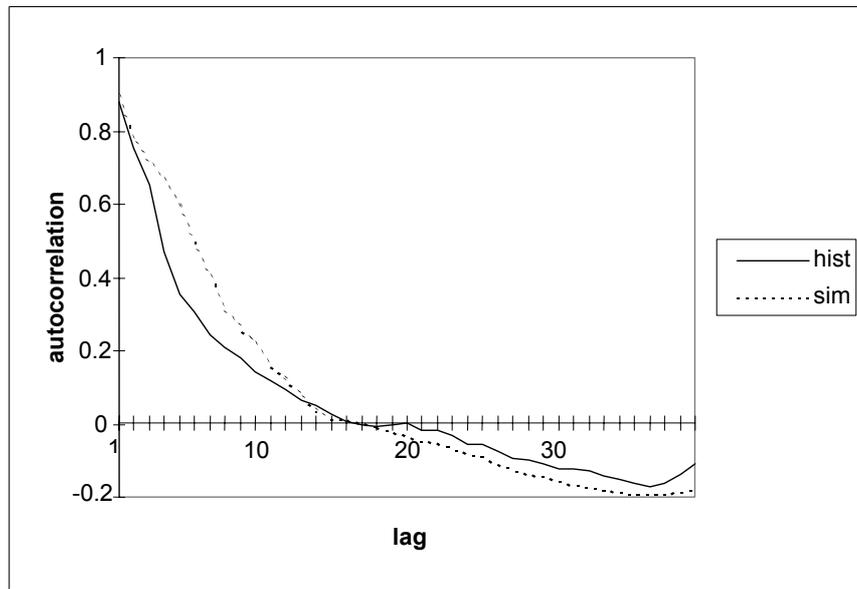


Figure 5: Correlogram of the most intense event

### Conclusions

The maximum rainfall intensity in a 5min interval can be simulated for a given hourly depth using the regression model described herein. The fitted regression model can be combined with the probability distribution function proposed by Ormsbee (1989) to disaggregate hourly rainfall into 5min values. This procedure corrects most of the negative bias in the maximum sub-hourly intensities, found when applying Ormsbee's method.

Overall, the results support the use of the model for applications in urban hydrology and in the design and upgrading of sewer systems.

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