Copyright is owned by the Author of the thesis. Permission is given for a copy to be downloaded by an individual for the purpose of research and private study only. The thesis may not be reproduced elsewhere without the permission of the Author.

Performance of a Transcritical Carbon Dioxide Heat Pump for Simultaneous Refrigeration and Water Heating

A thesis presented in partial fulfilment of the requirements for the degree of Master of Technology at Massey University.

Michael George Yarrall B.Tech. (Hon)

1998

ABSTRACT

Many industrial processes require both refrigeration to less than 0°C and water heating to greater than 60°C. Traditional independent refrigeration and boiler systems have relatively poor energy efficiency, whilst conventional heat pumps can provide both cooling and heating but are limited in terms of the temperature lift that can be achieved. A novel heat pump using CO₂ as the refrigerant in a transcritical cycle has been proposed as a new technology that can overcome these disadvantages. The use of CO₂ as a refrigerant has many advantages. It is environmentally benign, safe, and has good thermodynamic properties, especially compared with fluorocarbons. The transcritical cycle involves evaporation of CO₂ at constant temperature and pressure below the critical point to provide refrigeration, while cooling of the CO₂ occurs at temperatures and pressures above the critical point to provide heating of water. The objective of this project was to design and construct a prototype transcritical CO₂ heat pump to simultaneously provide refrigeration and water heating, and to test its performance over a wide range of operating conditions.

The prototype CO₂ heat pump had a nominal cooling capacity of 90 kW at -6°C and nominal water heating capacity of 127 kW from 10°C to 90°C. The prototype was designed to operate with a suction pressure of 30 bar and discharge pressure of 130 bar. The major components were a gas cooler, recuperator, flooded evaporator, low pressure separator/receiver, compressor, expansion valve, connecting piping and a control system. All components were standard high pressure equipment used by the natural gas processing industry. The gas cooler had a reasonably unique design to ensure close to pure counter-current heat exchange between the cooling CO₂ gas and the water being heated, both of which had relatively low flowrates. The compressor used was an open crankcase, reciprocating type with special gas seals on the piston rod to prevent CO₂ leakage. Refrigeration capacity (suction pressure) was controlled by varying the compressor speed. Water heating capacity was controlled by both using the expansion valve to control the CO₂ discharge pressure and varying the water flowrate through the gas cooler.

The main problem encountered during commissioning of the prototype was CO₂ leakage through the compressor piston rod seals. Alternative sealing systems were tried, but the leakage remained an on-going problem that prevented prolonged operation of the prototype, such as would be necessary in industrial applications.

Performance of the prototype was determined by energy balances based on measurements of CO₂ and water flowrate and temperature when it operated at steady-state. The energy balances generally agreed to within 6%. Trials were performed with suction pressures from 29.6 to 35.5 bar, discharge pressures from 80 to 130 bar, with hot water outlet temperatures from 65°C to 90°C, and evaporator water inlet temperatures from 11°C to 21°C.

When heating water to 90°C and providing refrigeration at 1°C (35.5 bar suction pressure), the maximum overall Coefficient of Performance (COP) achieved was 5.4 at a discharge pressure of 114 bar. Below this optimum discharge pressure, the COP

declined due to gas cooler heat transfer limitations (lower compressor discharge temperature led to lower temperature difference in the gas cooler and high CO₂ outlet temperature). Above the optimum, the decline in thermodynamic and compressor efficiency as pressure ratio increased caused the COP to decrease. The maximum heating and cooling capacities were about 13% less than the design values. This was attributed to the lower than expected volumetric efficiency of the compressor. The performance of the heat exchangers were generally close to the design values when allowances for lower than design water flowrates were taken into account.

As expected, when suction pressure was reduced to 29.6 bar (-6°C), there was up to a 10% decrease in optimum COP as well as reduced heating and cooling capacity. When heating water to 65°C rather than 90°C, the optimum COP was about 20% higher. When suction pressure or hot water outlet temperature was decreased, the optimum discharge pressure became slightly lower due to the gas cooler heat transfer being less of a limitation on overall system performance.

Addition of oil to the CO₂ did not reduce the CO₂ leakage sufficiently to allow long-term operation without recharging, and had minimum impact on the performance of the gas cooler, recuperator and compressor. However, oil fouling caused a significant drop in heat transfer performance of the evaporator.

The measured prototype performance agreed well with process simulations of the equipment and with results for similar laboratory scale equipment reported in the literature. Therefore, simulations could be used to optimise component and system design with a reasonable level of confidence. It was shown that the biggest increase in COP could be achieved by improving compressor isentropic efficiency rather than increased heat exchanger size.

Overall, the concept of the transcritical CO_2 heat pump for simultaneous refrigeration and water heating was proven and the required energy efficiency was sufficiently high that the heat pump is likely to be economically competitive with traditional heating and cooling systems. Further work should concentrate on improving compressor design to eliminate CO_2 leakage and to improve both isentropic and volumetric efficiency.

ACKNOWLEDGEMENTS

Thanks to all those who have helped me during the course of my degree, especially:

My supervisors, Don Cleland and Stephen White for all their help and for guiding me through the tough times.

Thanks to everyone at Flotech, including Chris Beh, Richard Hedley, Brett Rumble, Stephen Broadbent, Rodney Stephenson who helped me with my project.

Rodger Kallu for his help and advice.

My parents for their encouragement and support.

Finally, thank you to all those whom I may have inconvenienced by my misjudgement of when I was going to finish.

I also wish to acknowledge the help I received from the following foundations and scholarships:

Graduate Research in Industry Fellowship (Foundation for Research, Science and Technology)
IPENZ Craven Scholarship

Massey Masterate Scholarship

TABLE OF CONTENTS

Acknowl	edgements	iv
Table of	Contents	v
List of Fi	gures	viii
	ables	
1	INTRODUCTION	1
2	LITERATURE REVIEW	3
	Heat Pumps	
2.1.1	Conventional cycle	
	Environmental Aspects	
2.2.1	Fluorocarbons	
2.2.1.		
2.2.1.		
2.2.2		
2.2.2.		
2.3	Carbon Dioxide as a Refrigerant	
2.3.1	Advantages	
2.3.2		
2.4	Transcritical CO ₂ Process	11
2.4.1	Transcritical Heat Pump Cycle Description	
2.4.1.		
2.4.1.		
2.4.2	1985년 - 1985년 전 전 1987년 전 198	
	Applications and Performance Testing	
2.5.1	Process Performance - Simulated	
2.5.1.		
2.5.1.	시간 발생 이 어린 경영 전 프로그램이 프로그램 프로젝트 아내는 그 아내는 그 아내는	
2.5.1.		
2.5.1		
2.5.2		
2.5.2.		
2.5.2.		
2.5.3		
2.5.4		
2.5.4.		
2.5.4.		
2.5.4.		
2.5.4.		
2.6	Conclusions	30
3	OBJECTIVES	32
4	PROTOTYPE DESCRIPTION	33
	General Description	
	Process Description	
	Component Description	
4.3.1	8	
4.3.2		
4.3.3		
4.3.4	*	
4.3.5	Recuperator (Internal Heat Exchanger)	41

4.3.7	Piping	45
4.3.7.1	Thermosiphon	
4.3.7.2	Oil Return System	
4.3.8	Valves	
4.3.9	System Charge	
4.3.10	Compressor	
4.3.11	System Oil	
4.3.12	Motor and Drive	
	ontrol	
4.4.1	Refrigeration Control	
4.4.2	Water Heating Control	
4.4.2.1	Discharge Pressure Control	
4.4.2.2	Water Temperature Control	
4.4.2.2		
	PLC and Safety Controls	
4.4.3.1	Overview	
4.4.3.2	Switches	
4.4.3.3	Pressure Relief Valves	
	strumentation and Data Acquisition	
4.5.1	Temperature	
4.5.2	CO ₂ Flowrate	
4.5.3	Pressure	
4.5.3.1	Pressure Indicators	
4.5.3.2	Pressure Transducers	
4.5.4	Power Consumption	
4.5.5	Water Flowrate	
4.5.6	Data Acquisition	60
5 EY	(DEDIMENTAL DEOCEDLIDE	61
	(PERIMENTAL PROCEDURE	
5.1 Co	mmissioning and Preliminary Trials	61
5.1 Co 5.1.1	mmissioning and Preliminary Trials	61 61
5.1 Co 5.1.1 5.1.2	mmissioning and Preliminary Trials	61 61 63
5.1 Co 5.1.1 5.1.2 5.1.3	Commissioning and Preliminary Trials	61 63 63
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe	ommissioning and Preliminary Trials	61 61 63 63
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe	ommissioning and Preliminary Trials	61 63 63 64
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials	6163636465
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2 5.2.3	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature	616363646565
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4	Commissioning and Preliminary Trials Commissioning Start-Up Procedures. Shut Down Procedures. rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials.	61636364656568
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials	61636364656768
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials	6163636465676870
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da 5.3.1	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties	6163646568687070
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da 5.3.1 5.3.2	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties Gas Cooler Performance	6163646568687070
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate	6163646568707074
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures Formance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating	61636465687070707475
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3.3	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures Formance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance	616364656870707475
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3.3.1	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance Heat Transfer Rate Heat Transfer Rate	61636364656870707475
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3.1 5.3.3.1 5.3.3.2	Commissioning and Preliminary Trials Commissioning Start-Up Procedures. Shut Down Procedures. rformance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials. Oil Trials ta Analysis. Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating. Evaporator Performance Heat Transfer Rate Evaporator Rating.	6163646568687070747577
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Period of the second of t	Commissioning Start-Up Procedures Shut Down Procedures Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance Heat Transfer Rate Evaporator Performance Heat Transfer Rate Evaporator Performance Evaporator Performance Heat Transfer Rate Evaporator Performance Recuperator Performance Recuperator Performance Recuperator Performance Recuperator Performance	61636465686870707071757777
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.2.2 5.3.3.4 5.3.4.1	Start-Up Procedures Shut Down Procedures Fromance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating. Evaporator Performance Heat Transfer Rate Evaporator Rating. Recuperator Performance Heat Transfer Rate Evaporator Rating. Recuperator Performance Heat Transfer Rate	6163646568687070747577777779
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Period of the second of t	Commissioning and Preliminary Trials Commissioning	
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.2.2 5.3.3.4 5.3.4.1	Start-Up Procedures Shut Down Procedures Fromance Trials Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature Evaporator Design Condition Trials Oil Trials Thermodynamic and Transport Properties Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating. Evaporator Performance Heat Transfer Rate Evaporator Rating. Recuperator Performance Heat Transfer Rate Evaporator Rating. Recuperator Performance Heat Transfer Rate	
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Pe 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Da 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.3.2 5.3.4 5.3.4.1 5.3.4.2	Commissioning and Preliminary Trials Commissioning Start-Up Procedures	616364656870707475777778797979
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.3.2 5.3.4 5.3.4.1 5.3.4.2 5.3.5 5.3.6 5.3.7	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties. Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance Heat Transfer Rate Evaporator Performance Heat Transfer Rate Evaporator Rating Recuperator Performance Heat Transfer Rate Evaporator Rating Variable Speed Drive (VSD) and Motor Compressor Performance. Overall System Performance	616364656870707475777778797979808081
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.3.2 5.3.4 5.3.4.1 5.3.4.2 5.3.5 5.3.6	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties. Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance Heat Transfer Rate Evaporator Performance Heat Transfer Rate Evaporator Rating Recuperator Performance Heat Transfer Rate Evaporator Performance Heat Transfer Rate Compressor Performance Heat Transfer Rate Recuperator Performance Variable Speed Drive (VSD) and Motor Compressor Performance Overall System Performance Heat Losses and Gains	
5.1 Co 5.1.1 5.1.2 5.1.3 5.2 Per 5.2.1 5.2.2 5.2.3 5.2.4 5.2.5 5.3 Dar 5.3.1 5.3.2 5.3.2.1 5.3.2.2 5.3.3 5.3.3.1 5.3.3.2 5.3.4 5.3.4.1 5.3.4.2 5.3.5 5.3.6 5.3.7	Commissioning and Preliminary Trials Commissioning Start-Up Procedures Shut Down Procedures Constant Evaporator Water Flowrate Trials Constant Speed Trials Effect of Evaporator Water Flowrate and Inlet Temperature. Evaporator Design Condition Trials Oil Trials ta Analysis Thermodynamic and Transport Properties. Gas Cooler Performance Heat Transfer Rate Gas Cooler Heat Transfer Rating Evaporator Performance Heat Transfer Rate Evaporator Performance Heat Transfer Rate Evaporator Rating Recuperator Performance Heat Transfer Rate Evaporator Rating Variable Speed Drive (VSD) and Motor Compressor Performance. Overall System Performance	61636364656870707074757777787980818283

6	RESULTS AND DISCUSSION	
6.1	Commissioning and Preliminary Trials	
6.1.		
6.1.		
6.1.		
6.1.		
6.1.		
6.2	Component Performance	
6.2.		
6.2.		
6.2.		
6.2.		
6.3	System Performance	
6.3.		
6.3.		
6.3.		
6.3.		
6.3.		
6.4	Process Simulations	
6.4.		
6.4.		
6.5	Economic Viability	115
7	CONCLUSION	117
8	REFERENCES	119
9	NOMENCLATURE	125
9.1	Subscripts	126
3.1	Subscripts	
10	APPENDICES	
A.1 -	Thermosiphon Calculation	128
A.2 -	System Volume and Charge	130
A.3 -	PLC Ladder Logic Code	134
A.4 -	BWR Macro	138
	Enthalpy Calculations	
A.6 -	CO ₂ Property Equations	144
A 7 -	Saturated Water Equations	146
A.8 -	Entropy Calculations	147
Δ9-	Heat Loss Calculations	149
Δ 10	- Raw Data	151
0		ner om telegram mentelfallet for finish

List of Figures

Figure 2.1: Conventional Refrigeration / Heat Pump Cycle	
Figure 2.2: Pressure - Enthalpy diagrams for CO ₂ and R12 (Pettersen, 1995)	9
Figure 2.3: Transcritical CO ₂ Heat Pump General Set-up for Project	12
Figure 2.4: Pressure - Enthalpy Diagram for a Conventional Cycle	
Figure 2.5: Pressure - Enthalpy Diagram for a Transcritical Cycle	
Figure 2.6: Differences in condenser / cooler profiles for conventional and transcritical CO ₂ processes.	
Figure 2.7: Optimum High Side Pressure for COP (Nekså et al, 1997)	16
Figure 2.8: Flow circuit of the Transcritical CO ₂ Heat Pump used by Chumak et al (1996)	19
Figure 2.9: Optimum discharge Pressures for Various Hot Water Temperatures (Nekså et al, 1997)	
Figure 2.10: Compressor Model Based on Prototype Measurements (Enkemann and Kruse, 1997)	
Figure 4.1: General Arrangement for Prototype Transcritical CO ₂ Heat Pump	
Figure 4.2: Process Flow Diagram	
Figure 4.3: Mechanical Drawings for Gas Cooler Heat Exchanger	
Figure 4.4: Mechanical Drawings for Evaporator	
Figure 4.5: Mechanical Drawings for Recuperator	
Figure 4.6: Mechanical Drawings for Separator	
Figure 4.7: Schematic Diagram Showing the Knox Western TP65 Compressor	
Figure 4.8: Process and Instrumentation Diagram (P&ID)	
Figure 4.9: Data acquisition system	
Figure 5.1: Evaporator Water Supply System	
Figure 5.2: Calculation of Change in Enthalpy	
Figure 5.3: Comparison of Equations of State Enthalpy Predictions at 130 bar	76
Figure 5.4: Temperature Profile in Gas Cooler	. / 0
without oil in the system.	88
Figure 6.2: Evaporator heat transfer resistance as a function of evaporator water flowrate for trials with	00
and without oil in the system.	80
Figure 6.3: Evaporator heat transfer coefficient as a function of CO ₂ mass flowrate for trials with and	0,5
without oil in the system.	90
Figure 6.4: Evaporator CO ₂ side heat transfer resistance as a function of evaporator water flowrate for	70
trials with and without oil in the system	90
Figure 6.5: Recuperator heat transfer coefficient as a function of CO ₂ mass flowrate for trials with and	
without oil in the system.	91
Figure 6.6: Compressor Efficiencies for All Trials	
Figure 6.7: COP as a function of discharge pressure for various suction pressures, with constant	
evaporator water flowrate (90°C hot water).	94
Figure 6.8: (a) Discharge Temperature, and (b) Enthalpy at inlet to expansion valve as a function of	
Discharge Pressure for various suction pressures, with constant evaporator water flowrate (90°C h	ot
water)	
Figure 6.9: (a) Compressor speed, and (b) CO ₂ mass flowrate as a function of discharge pressure for	
various suction pressures, with constant evaporator water flowrate (90°C hot water)	96
Figure 6.10: Gas cooler heat load and compressor power as a function of discharge pressure for various	
suction pressures, with constant evaporator water flowrate (90°C hot water).	. 97
Figure 6.11: COP as a function of discharge pressure for various suction pressures, with constant	
evaporator water flowrate (65°C hot water).	
Figure 6.12: Gas Cooler Heat Load and Compressor power as a function of discharge pressure for varie	
suction pressures, with constant evaporator water flowrate (65°C hot water).	
Figure 6.13: COP as a function of discharge pressure for various hot water temperatures, with constant	
evaporator water flowrate (32.6 bar suction pressure)	100
Figure 6.14: COP as a function of discharge pressure for various suction pressures, with constant	101
compressor speed (90°C hot water).	
Figure 6.15: Gas cooler heat load and compressor power as a function of discharge pressure for various	
suction pressures, with constant compressor speed (90°C hot water)	102
Figure 6.16: COP as a function of discharge pressure for a 29.6 bar suction pressure, with constant compressor speed (65°C hot water).	102
compressor speed (05 C not water).	103

	Gas Cooler Heat Load and Compressor power as a function of discharge pressure for vario	
	pressures, with constant compressor speed (65°C hot water)	04
Figure 6.18:	COP as a function of discharge pressure for various evaporator water inlet temperatures	
	ar suction pressure)	
Figure 6.19:	COP as a function of discharge pressure for various hot water temperatures, for evaporator	
water c	onditions close to design conditions (32.6 bar suction pressure)	06
Figure 6.20:	COP as a function of discharge pressure, with 0.6 L/s evaporator water flowrate at 21°C an	d
32.6 ba	er suction pressure, producing 90°C hot water, with and without oil in the system	07
Figure 6.21:	Isentropic efficiency as a function of discharge pressure, for trials with 0.6 L/s evaporator	
water f	lowrate at 21°C and 32.6 bar suction pressure, producing 90°C hot water, with and without	
oil in th	ne system	80
Figure 6.22:	COP as a function of discharge pressure, with constant compressor speed and 32.6 bar	
suction	pressure, producing 90°C hot water, with and without oil in the system	09
Figure 6.23: 1	Isentropic efficiency as a function of discharge pressure, with constant compressor speed an	ıd
	er suction pressure, producing 90°C hot water, with and without oil in the system	09
	COP as a function of discharge pressure, with constant compressor speed and 29.6 bar	
	pressure, producing 65°C hot water, with and without oil in the system 1	
	COP as a function of discharge pressure, with 1.4 L/s evaporator water flowrate at 11°C an	
	er suction pressure, producing 90°C hot water, with and without oil in the system 1	10
0	Simulated COP as a function of discharge pressure for various suction pressures, with	
	nt evaporator water flowrate (90°C hot water)	11
	Simulated COP as a function of discharge pressure for various suction pressures, with	
	nt evaporator water flowrate (65°C hot water) 1	12
	Simulated COP as a function of discharge pressure for various suction pressures, with	
	nt evaporator water flowrate with constant CO2 mass flowrate (90°C hot water) 1	12
	Simulated gas cooler and compressor heat load as a function of discharge pressure for	
	suction pressures, with constant compressor speed with constant CO ₂ mass flowrate (90°C	
	ter)	
	Gas Cooler Temperature Profile	
	COP as a function of discharge pressure for temperature profile	
Figure 6.32:	Internal rate of return	16

List of Tables

Table 2.1: Characteristics and Properties of Some Refrigerants (Lorentzen, 1994a)	8
Table 2.2: Explanation of cycles on pressure-enthalpy diagrams	13
Table 2.3: Simulated and Measured Response of the Transcritical CO ₂ System (Skaugen and System)	vensson,
1998)	18
Table 4.1: Detailed Gas Cooler Specifications.	37
Table 4.2: Detailed Evaporator Specifications	39
Table 4.3: Detailed Recuperator Specifications	
Table 4.4: Detailed Separator Specifications	
Table 4.5: Pipe Sizes and Types	
Table 4.6: Valve Types and Positions at Start-Up	47
Table 4.7: Compressor Specifications	
Table 4.8: Lubrication Oil Specifications	49
Table 4.9: Discharge Pressure Control Equipment Specifications	
Table 4.10: Programmable Logic Controller and Expansion Unit Specifications	53
Table 4.11: Fault Delays Used by the PLC	
Table 4.12: Switch Specifications	55
Table 4.13: Pressure Relief Valve Specifications	55
Table 4.14: Temperature Indicator Locations and Specifications	56
Table 4.15: Mass Flow Meter Specifications	57
Table 4.16: Pressure Indicators	
Table 4.17: Sensit Pressure Transducer	
Table 4.18: Kamstrup - Metro Pressure Transmitter	58
Table 4.19: Power Consumption Monitoring	
Table 4.20: Water Meter Specifications	59
Table 4.21: Frequency Transmitter Specifications	59
Table 4.22: Data Logger Specifications	60
Table 5.1: Constant Evaporator Water Flowrate Trials	66
Table 5.2: Constant Speed Trials	
Table 5.3: Effect of Evaporator Water Flowrate and Inlet Temperature Trials	68
Table 5.4: Design Condition Trials	
Table 5.5: Performance Trials with Oil in System	
Table 5.6: Ratios of Log-Mean to True Mean Temperature Difference for the Gas Cooler with	a 10°C
Minimum Temperature Approach	76
Table 6.1: Optimum Discharge Pressure and COP for Constant Evaporator Water Flowrate Tria	als
Producing 90°C Hot Water	94
Table 6.2: Optimum discharge pressure and COP for constant evaporator flowrate trials produc	
hot water	
Table 6.3: Optimum Discharge Pressure and COP for Constant Compressor Speed Trials Produ	
Hot Water	
Table 6.4: Maximum Heating and Cooling Capacity for Constant Compressor Speed Trials Pro	
90°C Hot Water	
Table 6.5: Optimum Discharge Pressure, Optimum COP and Evaporator Heat Transfer Coeffic	
Evaporator Water Inlet Temperature Trials (35.5 bar suction pressure)	105

1 INTRODUCTION

The provision of heating and cooling is a very important function in many industrial processes. In New Zealand an estimated 4700 TJ of energy is used for heating to less than 100°C, and 4500 TJ of energy is used for refrigeration by the food processing industry each year (Kallu and Cleland, 1996). A large proportion of the heating is used to generate hot water for cleaning, sterilisation and other general process heating duties. Often the water needs to be at greater than 80°C due to food safety regulations and other process constraints. Most of the refrigeration is required at temperatures less than 10°C for preservation of food and other perishable products.

Traditionally, heating and refrigeration have been provided separately. This has several advantages. In particular, the amount of heating or refrigeration is easily controlled, and neither is dependent on the other. If only heating or cooling is required at any one time, separate systems are generally more cost efficient.

Cooling is usually provided by vapour compression refrigeration cycles, in which heat is usefully extracted at low temperatures and is rejected to the environment at higher temperatures. Refrigeration cycles at about 0°C typically provide about four times as much cooling as the energy required to drive the compressor.

Heating has been traditionally supplied by boilers. This can be quite cost effective when the price of the fuel for the boiler is low and temperatures greater than 80°C are required. The energy efficiency of boiler systems is typically between 50 and 80%.

An alternative to the use of boilers is passive heat recovery. This is only feasible when an existing process stream is available at sufficiently high temperature. For example, desuperheating of refrigerants after compression in refrigeration systems can provide high temperature heat, but the total heat available at high temperature is usually less than 15% of the total heat rejected from the refrigeration system (White *et al*, 1997). At most sites, there is a large number of options for heat recovery to achieve low temperatures (eg. less than 60°C), but relatively few for higher temperatures.

Another alternative are heat pumps which use the same cycle as refrigeration systems except that waste heat is extracted from the environment and it is the heat of rejection at higher temperatures that is useful. Traditional heat pumps can be energy efficient, typically giving two to six times as much heat as energy consumed (Hewitt *et al*, 1997). However they generally have a high capital cost, and are restricted in the temperatures they can deliver due to loss of efficiency at large temperature lifts and the pressure limitations of commonly available equipment. Conventional heat pumps often use fluorocarbons as the refrigerant, which are currently being phased out due to their ozone depleting and global warming effects.

The use of heat pumps enables the possibility of providing simultaneous heating and cooling. If the heat extracted by the heat pump system is also utilised for refrigeration, much greater overall energy efficiency is obtained. In addition, a single, integrated system requires less space and maintenance than the two separate systems.

Unfortunately, with most conventional heat pump and refrigeration systems, the large temperature split required to provide simultaneous heating and cooling at useful temperatures cannot be achieved without a large loss in efficiency.

Lorentzen (1994) proposed the transcritical carbon dioxide heat pump as a system which is able to efficiently provide high temperature process heat as well as simultaneous cooling. This technology has the potential to be more efficient and cost effective than present systems and also has the advantage of using CO₂ which is naturally occurring and environmentally friendly compared with fluorocarbon refrigerants.

The general objective for this project is to investigate the feasibility of utilising the transcritical CO₂ heat pump cycle for industrial heating and cooling. The project has been organised as part a joint venture between Flotech Ltd, Electricity Corporation of New Zealand Ltd (ECNZ), and Massey University.